

Normalizing VV at the LHC

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LES HOUCHES



Physics at TeV Colliders

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Normalizing VV with Z^(*)

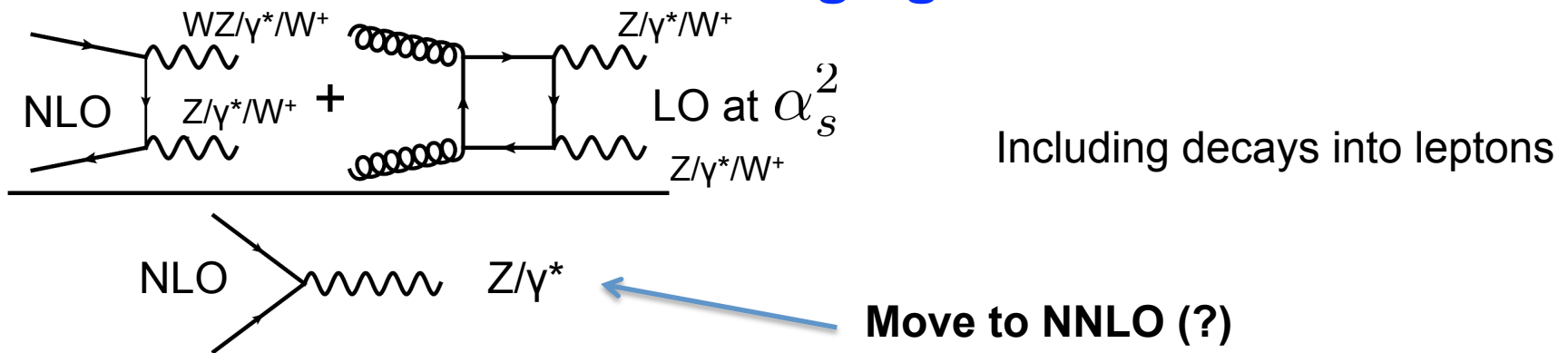
- **Strong similarities of diagrams since dominant cross-section comes from qq→V(V) via EW couplings**
- **Ratios VV/V expected to reduce pdf and a significant portion of the scale uncertainty**
 - **This is an asset especially at the very beginning of data taking when global pdf fits will not be available**

$$\begin{array}{cccc}
 \text{Prediction} & \text{Theory} & \text{Experimental} & \text{Observed} \\
 & & \text{efficiencies} & \\
 N(VV) = & \left(\frac{\sigma(pp \rightarrow VV)}{\sigma(pp \rightarrow Z^{(*)})} \right)_{Th} & \cdot \epsilon(ll \rightarrow Nl) & \cdot N_{Obs}(Z^{(*)})
 \end{array}$$

Ratio $ZZ(WW)/Z^{(*)}$

□ The production of ZZ and WW is enhanced by large contributions from $gg \rightarrow VV$ with gluons in the initial state

□ Formally a part of the NNLO contribution, but enhanced due to the large gluon flux



$$R = \frac{\sigma_{q\bar{q} \rightarrow ZZ, WW}^{NLO} + \sigma_{gg \rightarrow ZZ, WW}^{LO}}{\sigma_{q\bar{q} \rightarrow Z^{(*)}}^{NLO}}$$

Nominal Values of ZZ/Z*

- Ratios are constructed such that the invariant mass of Z* and ZZ are in the same bin
- Contribution from gg->ZZ increases sigma by ~13%
- Ratio depends weakly with Mass (nice surprise!)
 - Need to understand better behavior at very large masses

Cross-sections in fb

| Mass Range | $\sigma_{q\bar{q}\rightarrow Z^*}^{NLO}$ | $\sigma_{q\bar{q}\rightarrow ZZ}^{NLO}$ | $\sigma_{gg\rightarrow ZZ}^{LO}$ | $\frac{\sigma_{ZZ}}{\sigma_{Z^*}} \times 10^3$ |
|------------|--|---|----------------------------------|--|
| 200 - 250 | 1773.7 | 7.99 | 1.182 | 5.17 |
| 250 - 300 | 753.2 | 3.65 | 0.530 | 5.54 |
| 300 - 350 | 372.4 | 1.86 | 0.246 | 5.66 |
| 350 - 400 | 205.7 | 1.07 | 0.131 | 5.83 |
| 400 - 450 | 121.0 | 0.64 | 0.082 | 5.94 |
| 450 - 500 | 76.0 | 0.40 | 0.055 | 6.01 |
| 500 - 750 | 143.9 | 0.74 | 0.114 | 5.92 |
| 750 - 1000 | 27.4 | 0.16 | 0.033 | 6.88 |

Scale Errors of ZZ/Z*

- Treat qq->ZZ and gg->ZZ independently
 - Get maximum deviation by changing renormalization and factorization scales in opposite directions

| Mass Range | $\sigma_{q\bar{q}\rightarrow Z^*}^{NLO}$ | | $\sigma_{q\bar{q}\rightarrow ZZ}^{NLO}$ | | $\sigma_{gg\rightarrow ZZ}^{LO}$ | | $\frac{\sigma_{ZZ}}{\sigma_{Z^*}} \times 10^3$ | |
|------------|--|---------|---|---------|----------------------------------|---------|--|---------|
| | Value | % Error | Value | % Error | Value | % Error | Value | % Error |
| 200 - 250 | 1858.8 | 4.8 | 8.34 | 4.3 | 1.92 | 62.0 | 5.52 | 6.6 |
| | 1586.8 | -10.5 | 7.14 | -10.6 | 0.75 | -36.4 | 4.98 | -3.8 |
| 250 - 300 | 792.0 | 5.2 | 3.86 | 5.9 | 0.83 | 57.3 | 5.93 | 6.9 |
| | 683.8 | -9.2 | 3.32 | -9.0 | 0.35 | -33.9 | 5.36 | -3.3 |
| 300 - 350 | 390.5 | 4.9 | 1.94 | 4.2 | 0.38 | 53.6 | 5.94 | 4.9 |
| | 340.7 | -8.5 | 1.70 | -8.5 | 0.17 | -31.5 | 5.50 | -2.9 |
| 350 - 400 | 214.7 | 4.4 | 1.10 | 3.3 | 0.20 | 49.3 | 6.05 | 3.8 |
| | 195.3 | -5.0 | 0.96 | -10.0 | 0.09 | -29.8 | 5.40 | -7.5 |
| 400 - 450 | 125.8 | 4.0 | 0.67 | 5.8 | 0.12 | 46.0 | 6.31 | 6.2 |
| | 114.8 | -5.1 | 0.60 | -6.4 | 0.06 | -28.5 | 5.70 | -4.1 |
| 450 - 500 | 79.5 | 4.5 | 0.43 | 6.5 | 0.08 | 44.3 | 6.38 | 6.3 |
| | 72.4 | -4.8 | 0.38 | -6.0 | 0.04 | -26.7 | 5.78 | -3.8 |
| 500 - 750 | 147.6 | 2.6 | 0.78 | 5.9 | 0.16 | 40.9 | 6.39 | 7.8 |
| | 140.4 | -2.5 | 0.70 | -4.8 | 0.09 | -22.0 | 5.64 | -4.7 |
| 750 - 1000 | 28.1 | 2.6 | 0.16 | 2.0 | 0.04 | 30.1 | 7.17 | 4.2 |
| | 28.2 | 2.9 | 0.15 | -4.9 | 0.03 | -17.8 | 6.21 | -9.8 |

Change scale by *4, /4

Cross-sections in fb

Ratio WW/Z(*)

□ Scale-related uncertainties arise from changing scales by factors of 4 (*4,/4)

□ Pick biggest deviation of changing at the same time and in opposite directions

$M_{Z^*} > 185 \text{ GeV}$

| | (pb) | (fb) | (fb) | (fb) | | |
|------|---|---|--|-----------------------------------|---|------------------------------------|
| | $\sigma_{q\bar{q} \rightarrow Z}^{NLO}$ | $\sigma_{q\bar{q} \rightarrow Z^*}^{NLO}$ | $\sigma_{q\bar{q} \rightarrow WW}^{NLO}$ | $\sigma_{gg \rightarrow WW}^{LO}$ | $\frac{\sigma_{WW}}{\sigma_Z} \cdot 10^3$ | $\frac{\sigma_{WW}}{\sigma_{Z^*}}$ |
| Nom. | 785.3 | 2256.4 | 636.0 | 31.04 | 0.85 | 0.296 |
| Max. | 6.2 | 4.6 | 11.5 | 62.1 | 16.1 | 9.4 |
| Min. | -15.7 | -9.9 | -13.4 | -36.0 | -8.4 | -5.3 |

Same as above after multiplying $\sigma(gg \rightarrow WW)$ by two

| | $\sigma_{q\bar{q} \rightarrow Z}^{NLO}$ | $\sigma_{q\bar{q} \rightarrow Z^*}^{NLO}$ | $\sigma_{q\bar{q} \rightarrow WW}^{NLO}$ | $\sigma_{gg \rightarrow WW}^{LO}$ | $\frac{\sigma_{WW}}{\sigma_Z} \cdot 10^3$ | $\frac{\sigma_{WW}}{\sigma_{Z^*}}$ |
|------|---|---|--|-----------------------------------|---|------------------------------------|
| Nom. | 785.3 | 2256.4 | 636.0 | 62.08 | 0.89 | 0.309 |
| Max. | 6.2 | 4.6 | 11.5 | 62.1 | 19.2 | 12.0 |
| Min. | -15.7 | -9.9 | -13.4 | -36.0 | -10.2 | -6.7 |

Ratio ZW/Z(*)

Ratio evaluated to NLO

For ZW require P_T or leading lepton to be >20 and the two sub-leading, >10 GeV

\sqrt{s} dependence of ratios evaluated

$$R = \frac{\sigma_{q\bar{q} \rightarrow ZW}^{NLO}}{\sigma_{q\bar{q} \rightarrow Z^{(*)}}^{NLO}}$$

$M_{Z^*} > 195$ GeV

| | $\sigma_{q\bar{q} \rightarrow Z^*}^{NLO}$ | $\sigma_{q\bar{q} \rightarrow ZW}^{NLO}$ | $\frac{\sigma_{ZW}}{\sigma_Z} \cdot 10^3$ | $\frac{\sigma_{ZW}}{\sigma_{Z^*}}$ |
|---------|---|--|---|------------------------------------|
| Nominal | 1898.4 | 92.5 | 0.118 | 0.0487 |
| Maximum | 4.6 | 12.9 | 16.0 | 7.9 |
| Minimum | -9.2 | -12.0 | -11.3 | -6.5 |

\sqrt{s} Dependence

- **The Ratio ZZ/Z^* seems to be flat as a function of \sqrt{s} and different mass ranges**
 - **The ratio ZZ/Z is less flat**

| \sqrt{s} | 200 – 250 | 250 – 300 | 300 – 500 | 500 – 1000 |
|------------|-----------|-----------|-----------|------------|
| 14 | 5.17 | 5.54 | 5.79 | 6.08 |
| 10 | 4.98 | 5.33 | 5.48 | 5.61 |
| 8 | 4.92 | 5.24 | 5.34 | 5.53 |

Flatness of ratio indicates reduction of pdf uncertainties

PDF Uncertainties (ratios)

□ Use CTEQ6.1 and evaluate the 40 pdf checks

□ Results depends weakly on cms energy

Uncertainties in %

| \sqrt{s} | $\delta \frac{\sigma(ZZ)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZZ)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z^*)}$ |
|------------|---------------------------------------|---|---------------------------------------|---|---------------------------------------|---|
| 14 | 1.4 | 0.5 | 1.3 | 0.3 | 1.4 | 0.4 |
| 10 | 1.5 | 0.5 | 1.4 | 0.3 | 1.4 | 0.5 |
| 8 | 1.5 | 0.6 | 1.4 | 0.3 | 1.5 | 0.6 |

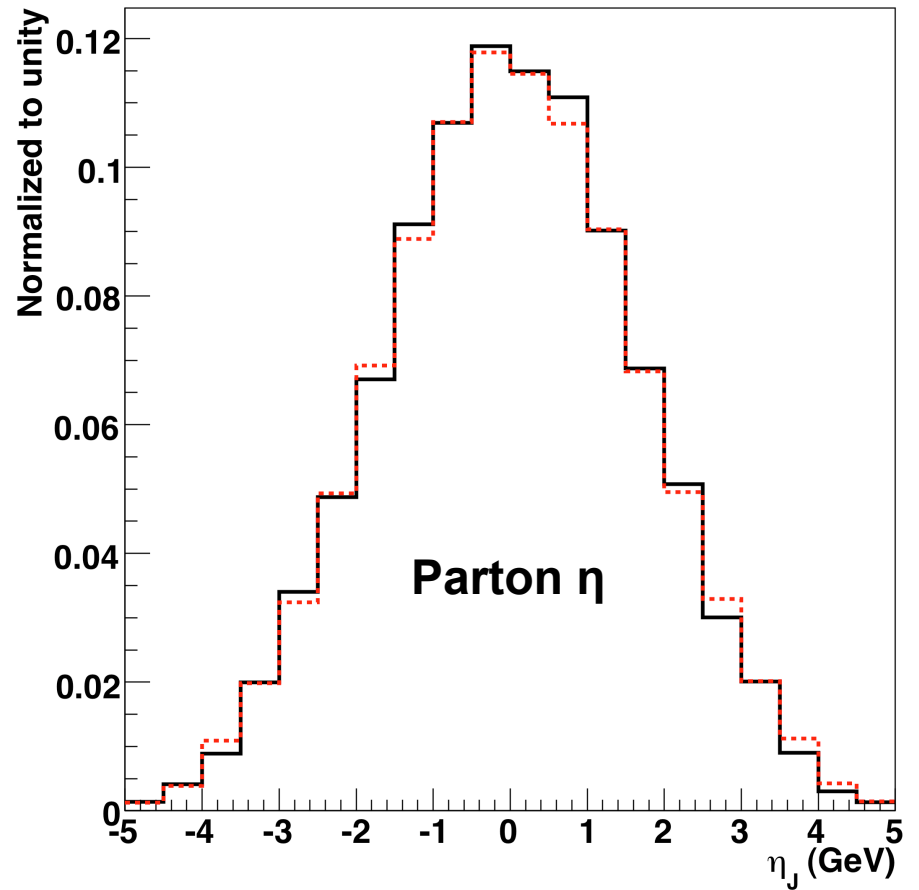
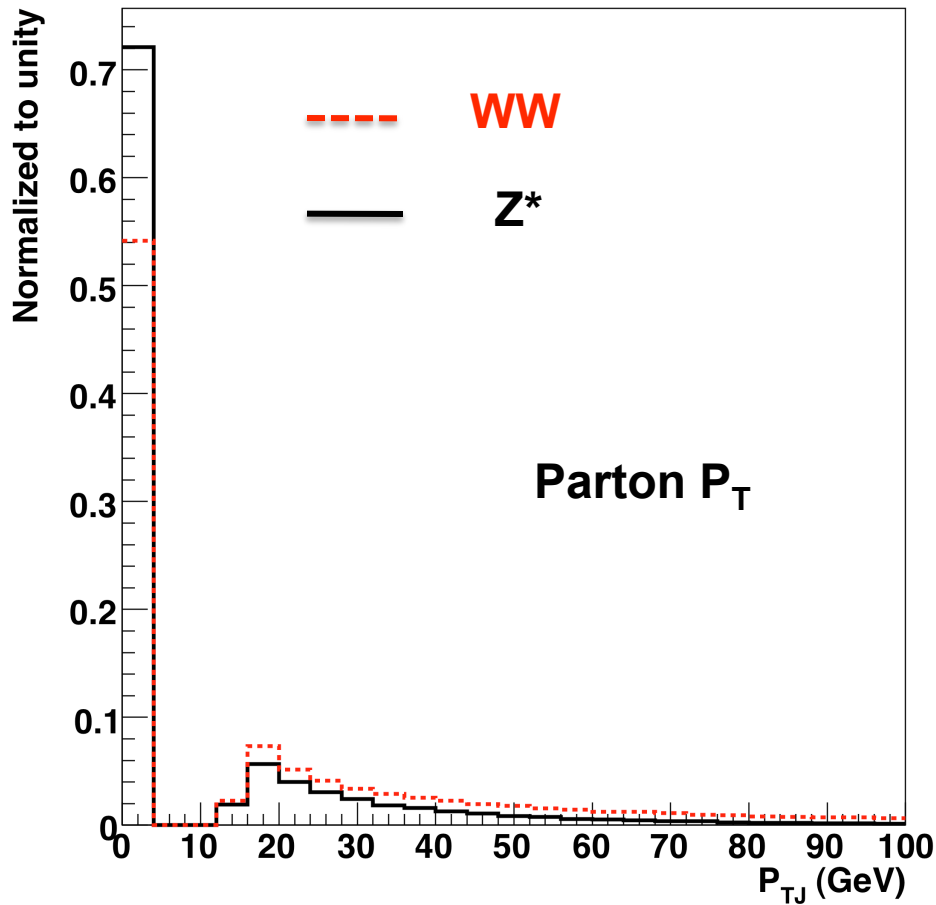
Shown errors on ratios to NLO

□ Pdf-related errors of VV are more correlated with Z* and with Z

| Check | $\delta \frac{\sigma(ZZ)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZZ)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z^*)}$ |
|-------|---------------------------------------|---|---------------------------------------|---|---------------------------------------|---|
| 1 | 0.0 | -0.3 | 0.2 | -0.1 | 0.3 | 0.0 |
| 2 | 0.0 | 0.3 | -0.2 | 0.1 | -0.3 | 0.0 |
| 3 | 0.6 | 0.2 | 0.6 | 0.2 | 0.7 | 0.3 |
| 4 | -0.5 | -0.2 | -0.6 | -0.2 | -0.7 | -0.3 |
| 5 | -0.6 | 0.0 | -0.6 | 0.0 | -0.7 | -0.1 |
| 6 | 0.6 | 0.0 | 0.6 | 0.0 | 0.7 | 0.1 |
| 7 | -0.9 | -0.3 | -0.7 | -0.1 | -0.8 | -0.2 |
| 8 | 0.9 | 0.3 | 0.7 | 0.1 | 0.8 | 0.1 |
| 9 | 1.0 | 0.0 | 1.1 | 0.1 | 1.2 | 0.2 |
| 10 | -1.2 | 0.0 | -1.3 | -0.1 | -1.4 | -0.3 |
| 11 | -0.6 | -0.2 | -0.5 | -0.2 | -0.6 | -0.3 |
| 12 | 0.5 | 0.3 | 0.5 | 0.2 | 0.5 | 0.3 |
| 13 | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | -0.1 |
| 14 | -0.1 | 0.0 | -0.1 | 0.0 | 0.0 | 0.1 |
| 15 | -0.1 | 0.0 | 0.0 | 0.1 | -0.1 | 0.0 |
| 16 | 0.1 | -0.1 | 0.1 | -0.1 | 0.2 | 0.0 |
| 17 | 0.6 | 0.3 | 0.5 | 0.1 | 0.5 | 0.2 |
| 18 | -0.7 | -0.4 | -0.4 | -0.2 | -0.4 | -0.2 |
| 19 | 0.6 | 0.0 | 0.5 | -0.1 | 0.4 | -0.2 |
| 20 | -0.7 | 0.0 | -0.6 | 0.1 | -0.6 | 0.1 |
| 21 | -0.4 | -0.1 | -0.5 | -0.1 | -0.6 | -0.2 |
| 22 | -0.8 | 0.1 | -0.8 | 0.0 | -0.9 | 0.0 |
| 23 | 0.1 | 0.3 | -0.1 | 0.1 | -0.1 | 0.1 |
| 24 | -0.1 | 0.1 | -0.2 | 0.0 | -0.3 | -0.1 |
| 25 | 0.3 | 0.3 | 0.2 | 0.1 | 0.2 | 0.1 |
| 26 | -0.4 | 0.0 | -0.4 | 0.0 | -0.4 | 0.0 |
| 27 | 0.2 | 0.1 | 0.2 | 0.1 | 0.3 | 0.2 |
| 28 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.1 |
| 29 | -0.4 | 0.0 | -0.3 | 0.1 | -0.3 | 0.2 |
| 30 | 1.0 | 0.1 | 0.9 | 0.1 | 1.0 | 0.2 |
| 31 | 0.0 | 0.2 | -0.1 | 0.0 | -0.2 | -0.1 |
| 32 | 0.0 | 0.3 | -0.2 | 0.1 | -0.2 | 0.1 |
| 33 | -0.3 | 0.3 | -0.4 | 0.1 | -0.5 | 0.1 |
| 34 | 0.4 | 0.3 | 0.2 | 0.1 | 0.1 | 0.0 |
| 35 | 0.1 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 |
| 36 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| 37 | -0.1 | 0.2 | -0.1 | 0.1 | -0.1 | 0.1 |
| 38 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 39 | 0.1 | 0.4 | -0.1 | 0.2 | 0.0 | 0.3 |
| 40 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 0.2 |
| Total | 1.4 | 0.5 | 1.3 | 0.3 | 1.4 | 0.4 |

Jet veto survival probability

$$\epsilon(p_T) = \frac{\sigma(p_{Tj}, p_{Tj} < p_T)}{\sigma}$$



$\sqrt{s} = 14 \text{ TeV}$

| p_T [GeV] | $\epsilon(Z^*)$ | $\delta\epsilon(Z^*)$ | $\epsilon(WW)$ | $\delta\epsilon(WW)$ | $\frac{\epsilon(WW)}{\epsilon(Z^*)}$ | $\delta\frac{\epsilon(WW)}{\epsilon(Z^*)}$ |
|---------------|-----------------|-----------------------|----------------|----------------------|--------------------------------------|--|
| 20 | 0.67 | 8.5 -13.2 | 0.52 | 11.9 -15.2 | 0.78 | 5.1 -3.2 |
| 25 | 0.72 | 6.4 -9.9 | 0.58 | 9.6 -11.8 | 0.81 | 4.0 -2.9 |
| 30 | 0.76 | 5.1 -7.8 | 0.63 | 8.3 -9.1 | 0.82 | 3.6 -2.1 |
| 35 | 0.79 | 4.1 -6.3 | 0.67 | 7.4 -7.3 | 0.84 | 3.3 -2.1 |
| 40 | 0.82 | 3.5 -5.3 | 0.70 | 6.6 -5.9 | 0.85 | 3.0 -1.9 |

 $\sqrt{s} = 10 \text{ TeV}$

| p_T [GeV] | $\epsilon(Z^*)$ | $\delta\epsilon(Z^*)$ | $\epsilon(WW)$ | $\delta\epsilon(WW)$ | $\frac{\epsilon(WW)}{\epsilon(Z^*)}$ | $\delta\frac{\epsilon(WW)}{\epsilon(Z^*)}$ |
|---------------|-----------------|-----------------------|----------------|----------------------|--------------------------------------|--|
| 20 | 0.69 | 8.6 -7.2 | 0.58 | 10.9 -13.5 | 0.83 | 2.1 -7.8 |
| 25 | 0.75 | 6.8 -5.5 | 0.63 | 9.2 -10.9 | 0.85 | 2.2 -6.3 |
| 30 | 0.78 | 5.6 -4.3 | 0.68 | 8.0 -9.8 | 0.86 | 2.2 -5.8 |
| 35 | 0.81 | 4.8 -3.7 | 0.71 | 7.1 -9.0 | 0.87 | 2.1 -5.4 |
| 40 | 0.84 | 4.1 -3.3 | 0.74 | 6.2 -8.1 | 0.88 | 2.0 -4.9 |

EXTRA SLIDES

MCFM Settings

| Parameter | Name (_inp) | Input Value | Output Value determined by <code>ewscheme</code> | | | |
|-------------------|----------------|--------------------------|--|------------|------------|------------|
| | | | -1 | 0 | 1 | 2 |
| G_F | Gf | 1.16639×10^{-5} | input | calculated | input | input |
| $\alpha(M_Z)$ | aemz | 1/128.89 | input | input | calculated | input |
| $\sin^2 \theta_w$ | xw | 0.2312 | calculated | input | calculated | input |
| M_W | wmass | 80.419 GeV | input | calculated | input | calculated |
| M_Z | zmass | 91.188 GeV | input | input | input | calculated |
| m_t | mt | 172.5 GeV | calculated | input | input | input |

| Parameter | Fortran name | Default value |
|---------------|--------------|-----------------------------|
| m_τ | mtau | 1.777 GeV |
| m_τ^2 | mtausq | 3.1577 GeV ² |
| m_c^2 | mcsq | 2.25 GeV ² |
| m_b^2 | mbsq | 17.64 GeV ² |
| Γ_τ | tauwidth | 2.269×10^{-12} GeV |
| Γ_W | wwidth | 2.06 GeV |
| Γ_Z | zwidth | 2.49 GeV |
| V_{ud} | Vud | 0.975 |
| V_{us} | Vus | 0.222 |
| V_{ub} | Vub | 0. |
| V_{cd} | Vcd | 0.222 |
| V_{cs} | Vcs | 0.975 |
| V_{cb} | Vcb | 0. |

Ratio WW/ZZ

- The ratio WW/ZZ will diminish the error due to the gg->VV contribution.
 - The errors will probably be dominated by the experimental uncertainties

| σ_{WW} | $\delta\sigma_{WW}$ | σ_{ZZ} | $\delta\sigma_{ZZ}$ | $\frac{\sigma_{ZZ}}{\sigma_{WW}} \cdot 10^2$ | $\delta \frac{\sigma_{ZZ}}{\sigma_{WW}}$ |
|---------------|---------------------|---------------|---------------------|--|--|
| 667.0 | 13.9 | 11.51 | 10.9 | 1.73 | 1.6 |
| | -14.4 | | -13.1 | | -2.6 |

- Results above include gg->WW

\sqrt{s} Dependence of WW/Z^*

□ Results reported to NLO and

□ Results were obtained with a dynamic scale

▪ (E_T of the weak-boson system)

| $\frac{\sigma(WW)}{\sigma(Z^*)}$ | \sqrt{s} [TeV] | $200 < M_{WW} < 250$ | $250 < M_{WW} < 300$ | $300 < M_{WW} < 500$ | $M_{WW} > 500$ |
|----------------------------------|------------------|----------------------|----------------------|----------------------|----------------|
| | 14 | 0.20 | 0.27 | 0.33 | 0.391 |
| | 12 | 0.20 | 0.26 | 0.33 | 0.388 |
| | 10 | 0.20 | 0.26 | 0.32 | 0.382 |
| | 8 | 0.19 | 0.25 | 0.31 | 0.385 |
| | 6 | 0.18 | 0.24 | 0.30 | 0.406 |

| $\frac{\sigma(WW)}{\sigma(Z)} \times 10^3$ | \sqrt{s} [TeV] | $200 < M_{WW} < 250$ | $250 < M_{WW} < 300$ | $300 < M_{WW} < 500$ | $M_{WW} > 500$ |
|--|------------------|----------------------|----------------------|----------------------|----------------|
| | 14 | 0.22 | 0.13 | 0.16 | 0.044 |
| | 12 | 0.22 | 0.12 | 0.16 | 0.040 |
| | 10 | 0.21 | 0.12 | 0.14 | 0.036 |
| | 8 | 0.20 | 0.11 | 0.13 | 0.030 |
| | 6 | 0.18 | 0.10 | 0.11 | 0.022 |

\sqrt{s} Dependence of VV/Z^*

□ Ratios are relatively stable w.r.t. \sqrt{s}

Results to NLO

| \sqrt{s} [TeV] | $\frac{\sigma(WW)}{\sigma(Z^*)}$ | $\frac{\sigma(ZW)}{\sigma(Z^*)}$ | $\frac{\sigma(ZZ)}{\sigma(Z^*)}$ |
|-------------------|----------------------------------|----------------------------------|----------------------------------|
| 14 | 0.280 | .0481 | .0063 |
| 12 | 0.294 | .0473 | .0062 |
| 10 | 0.271 | .0462 | .0062 |
| 8 | 0.265 | .0452 | .0062 |
| 6 | 0.256 | .0435 | .0062 |

PDF Uncertainties

□ Use CTEQ6.1 and evaluate the 40 pdf checks

□ Results depends weakly on cms energy

Uncertainties in %

| \sqrt{s} | $\delta\sigma(Z)$ | $\delta\sigma(Z^*)$ | $\delta\sigma(ZZ)$ | $\delta\sigma(WW)$ | $\delta\sigma(ZW)$ |
|------------|-------------------|---------------------|--------------------|--------------------|--------------------|
| 14 | 3.3 | 3.1 | 3.3 | 3.0 | 2.8 |
| 10 | 3.3 | 3.2 | 3.4 | 3.1 | 2.9 |
| 8 | 3.4 | 3.4 | 3.5 | 3.2 | 3.0 |

Shown errors on cross-sections to NLO

| Check | $\delta\sigma(Z)$ | $\delta\sigma(Z^*)$ | $\delta\sigma(ZZ)$ | $\delta\sigma(WW)$ | $\delta\sigma(ZW)$ |
|-------|-------------------|---------------------|--------------------|--------------------|--------------------|
| 1 | -1.2 | -1.0 | -1.2 | -1.0 | -0.9 |
| 2 | 1.2 | 1.0 | 1.2 | 1.0 | 0.9 |
| 3 | -1.3 | -1.0 | -0.8 | -0.8 | -0.7 |
| 4 | 1.3 | 1.0 | 0.8 | 0.8 | 0.7 |
| 5 | 0.0 | -0.6 | -0.6 | -0.6 | -0.6 |
| 6 | -0.1 | 0.5 | 0.6 | 0.5 | 0.6 |
| 7 | -0.2 | -0.8 | -1.1 | -0.9 | -1.0 |
| 8 | 0.1 | 0.8 | 1.1 | 0.9 | 0.9 |
| 9 | -2.1 | -1.1 | -1.1 | -1.0 | -0.9 |
| 10 | 2.3 | 1.1 | 1.1 | 1.0 | 0.8 |
| 11 | 1.2 | 0.9 | 0.6 | 0.7 | 0.6 |
| 12 | -1.1 | -0.8 | -0.6 | -0.6 | -0.6 |
| 13 | 0.3 | 0.4 | 0.4 | 0.4 | 0.3 |
| 14 | -0.3 | -0.4 | -0.3 | -0.3 | -0.3 |
| 15 | -0.6 | -0.7 | -0.7 | -0.6 | -0.7 |
| 16 | 0.1 | 0.3 | 0.2 | 0.2 | 0.3 |
| 17 | -0.2 | 0.1 | 0.4 | 0.3 | 0.3 |
| 18 | -0.2 | -0.5 | -0.8 | -0.6 | -0.6 |
| 19 | 1.3 | 1.8 | 1.9 | 1.8 | 1.7 |
| 20 | -1.0 | -1.7 | -1.7 | -1.6 | -1.6 |
| 21 | 1.3 | 1.0 | 0.9 | 0.9 | 0.8 |
| 22 | 0.3 | -0.6 | -0.5 | -0.6 | -0.6 |
| 23 | 0.7 | 0.5 | 0.8 | 0.6 | 0.6 |
| 24 | 1.1 | 0.9 | 0.9 | 0.8 | 0.8 |
| 25 | 0.1 | 0.2 | 0.5 | 0.3 | 0.3 |
| 26 | 0.2 | -0.2 | -0.2 | -0.2 | -0.2 |
| 27 | -0.8 | -0.7 | -0.6 | -0.6 | -0.5 |
| 28 | -0.8 | -0.9 | -0.9 | -0.9 | -0.8 |
| 29 | 0.2 | -0.2 | -0.2 | -0.1 | -0.1 |
| 30 | -2.8 | -1.9 | -1.8 | -1.8 | -1.7 |
| 31 | 0.9 | 0.8 | 0.9 | 0.8 | 0.7 |
| 32 | 1.0 | 0.7 | 1.0 | 0.8 | 0.8 |
| 33 | 1.1 | 0.6 | 0.9 | 0.7 | 0.7 |
| 34 | 0.4 | 0.5 | 0.8 | 0.6 | 0.5 |
| 35 | -0.8 | -0.8 | -0.7 | -0.7 | -0.6 |
| 36 | -0.9 | -0.9 | -0.8 | -0.8 | -0.8 |
| 37 | -1.0 | -1.2 | -1.1 | -1.1 | -1.1 |
| 38 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 39 | -0.1 | -0.4 | 0.0 | -0.2 | -0.1 |
| 40 | 0.0 | -0.1 | 0.1 | 0.0 | 0.0 |
| Total | 3.3 | 3.1 | 3.3 | 3.0 | 2.8 |

PDF Uncertainties (ratios)

□ Use CTEQ6.1 and evaluate the 40 pdf checks

□ Results depends weakly on cms energy

Uncertainties in %

| \sqrt{s} | $\delta \frac{\sigma(ZZ)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZZ)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z^*)}$ |
|------------|---------------------------------------|---|---------------------------------------|---|---------------------------------------|---|
| 14 | 1.4 | 0.5 | 1.3 | 0.3 | 1.4 | 0.4 |
| 10 | 1.5 | 0.5 | 1.4 | 0.3 | 1.4 | 0.5 |
| 8 | 1.5 | 0.6 | 1.4 | 0.3 | 1.5 | 0.6 |

Shown errors on ratios to NLO

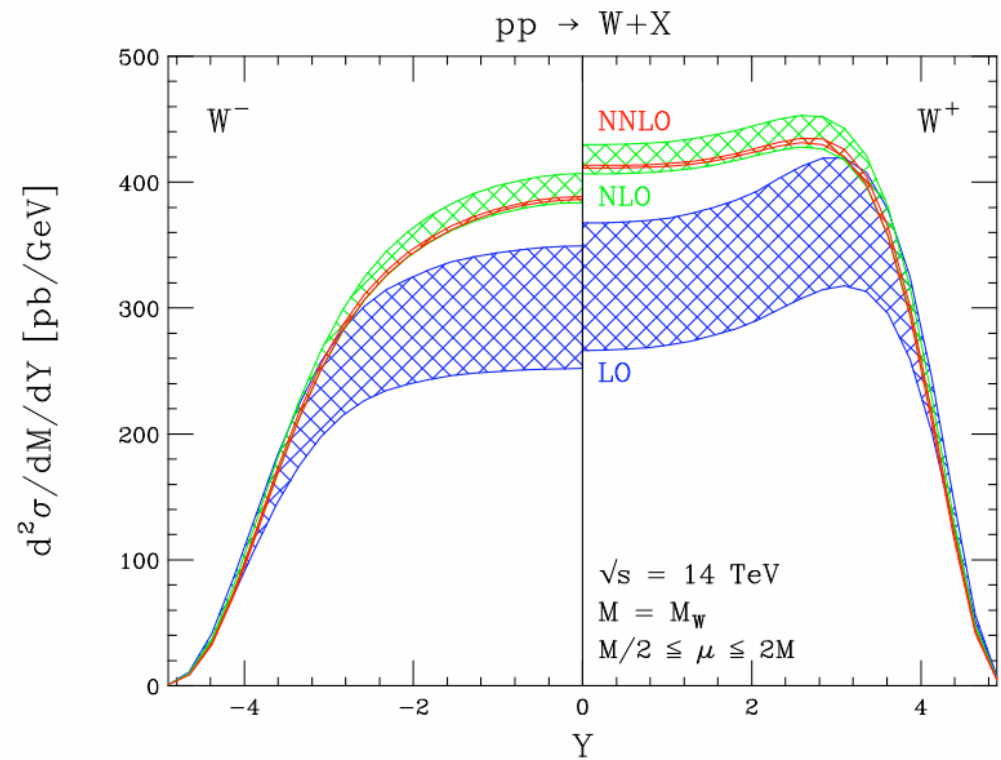
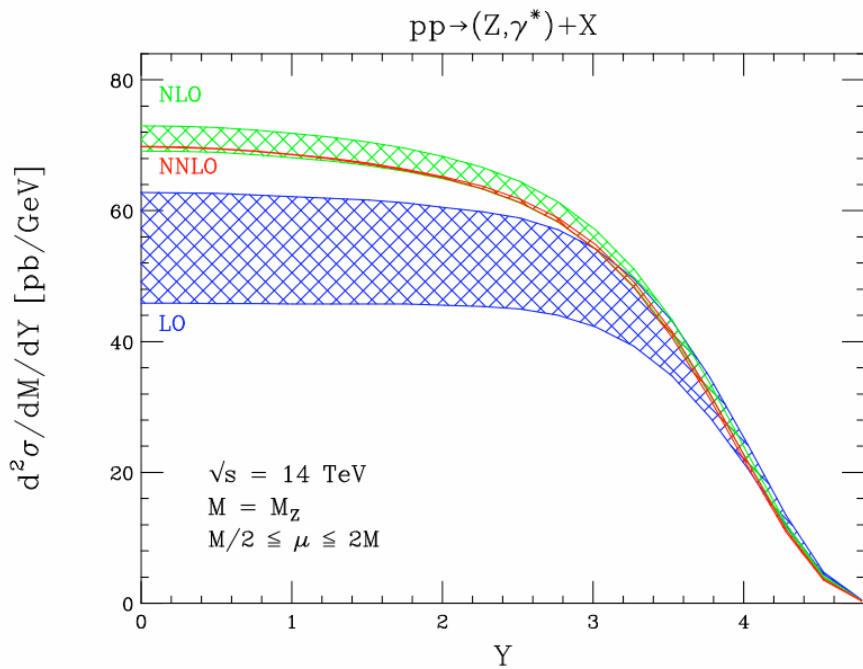
□ Pdf-related errors of VV are more correlated with Z* and with Z

| Check | $\delta \frac{\sigma(ZZ)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZZ)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z)}$ | $\delta \frac{\sigma(WW)}{\sigma(Z^*)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z)}$ | $\delta \frac{\sigma(ZW)}{\sigma(Z^*)}$ |
|-------|---------------------------------------|---|---------------------------------------|---|---------------------------------------|---|
| 1 | 0.0 | -0.3 | 0.2 | -0.1 | 0.3 | 0.0 |
| 2 | 0.0 | 0.3 | -0.2 | 0.1 | -0.3 | 0.0 |
| 3 | 0.6 | 0.2 | 0.6 | 0.2 | 0.7 | 0.3 |
| 4 | -0.5 | -0.2 | -0.6 | -0.2 | -0.7 | -0.3 |
| 5 | -0.6 | 0.0 | -0.6 | 0.0 | -0.7 | -0.1 |
| 6 | 0.6 | 0.0 | 0.6 | 0.0 | 0.7 | 0.1 |
| 7 | -0.9 | -0.3 | -0.7 | -0.1 | -0.8 | -0.2 |
| 8 | 0.9 | 0.3 | 0.7 | 0.1 | 0.8 | 0.1 |
| 9 | 1.0 | 0.0 | 1.1 | 0.1 | 1.2 | 0.2 |
| 10 | -1.2 | 0.0 | -1.3 | -0.1 | -1.4 | -0.3 |
| 11 | -0.6 | -0.2 | -0.5 | -0.2 | -0.6 | -0.3 |
| 12 | 0.5 | 0.3 | 0.5 | 0.2 | 0.5 | 0.3 |
| 13 | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | -0.1 |
| 14 | -0.1 | 0.0 | -0.1 | 0.0 | 0.0 | 0.1 |
| 15 | -0.1 | 0.0 | 0.0 | 0.1 | -0.1 | 0.0 |
| 16 | 0.1 | -0.1 | 0.1 | -0.1 | 0.2 | 0.0 |
| 17 | 0.6 | 0.3 | 0.5 | 0.1 | 0.5 | 0.2 |
| 18 | -0.7 | -0.4 | -0.4 | -0.2 | -0.4 | -0.2 |
| 19 | 0.6 | 0.0 | 0.5 | -0.1 | 0.4 | -0.2 |
| 20 | -0.7 | 0.0 | -0.6 | 0.1 | -0.6 | 0.1 |
| 21 | -0.4 | -0.1 | -0.5 | -0.1 | -0.6 | -0.2 |
| 22 | -0.8 | 0.1 | -0.8 | 0.0 | -0.9 | 0.0 |
| 23 | 0.1 | 0.3 | -0.1 | 0.1 | -0.1 | 0.1 |
| 24 | -0.1 | 0.1 | -0.2 | 0.0 | -0.3 | -0.1 |
| 25 | 0.3 | 0.3 | 0.2 | 0.1 | 0.2 | 0.1 |
| 26 | -0.4 | 0.0 | -0.4 | 0.0 | -0.4 | 0.0 |
| 27 | 0.2 | 0.1 | 0.2 | 0.1 | 0.3 | 0.2 |
| 28 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.1 |
| 29 | -0.4 | 0.0 | -0.3 | 0.1 | -0.3 | 0.2 |
| 30 | 1.0 | 0.1 | 0.9 | 0.1 | 1.0 | 0.2 |
| 31 | 0.0 | 0.2 | -0.1 | 0.0 | -0.2 | -0.1 |
| 32 | 0.0 | 0.3 | -0.2 | 0.1 | -0.2 | 0.1 |
| 33 | -0.3 | 0.3 | -0.4 | 0.1 | -0.5 | 0.1 |
| 34 | 0.4 | 0.3 | 0.2 | 0.1 | 0.1 | 0.0 |
| 35 | 0.1 | 0.1 | 0.2 | 0.1 | 0.2 | 0.1 |
| 36 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 |
| 37 | -0.1 | 0.2 | -0.1 | 0.1 | -0.1 | 0.1 |
| 38 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 39 | 0.1 | 0.4 | -0.1 | 0.2 | 0.0 | 0.3 |
| 40 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 0.2 |
| Total | 1.4 | 0.5 | 1.3 | 0.3 | 1.4 | 0.4 |

Pdf errors for gg->WW

- Independent study of pdf errors on gg->WW with various versions of CTEQ**
 - Obtain an errors of 5-10% to the total cross-section of gg->WW with CTEQ6**
 - This is significantly smaller than the scale-driven uncertainties**
- We did not investigate the correlations of the pdf errors of the qq,qg initial states with those of the gg initial states and the resulting effect on the ratio**
 - This is homework for the future**

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The NLO band does contain the NNLO result for Z, W^+, W^- production
Same applies for the $gg \rightarrow H$ production

\sqrt{s} Dependence of Jet Veto

Results of ϵ shown for $P_T=30$ GeV

| \sqrt{s} | WW | | | Z^* | | | $\frac{\epsilon_{jv}^{WW}}{\epsilon_{jv}^{Z^*}}$ |
|------------|-----------------------|--------------------------|-----------------|-----------------------|--------------------------|-----------------|--|
| | $\langle p_T \rangle$ | $\langle \eta \rangle$ | ϵ_{jv} | $\langle p_T \rangle$ | $\langle \eta \rangle$ | ϵ_{jv} | |
| 14 | 42.0 | 0.78 | 0.63 | 23.9 | 0.58 | 0.76 | 0.82 |
| 10 | 34.6 | 0.68 | 0.68 | 21.0 | 0.53 | 0.78 | 0.86 |
| 8 | 30.1 | 0.62 | 0.71 | 18.1 | 0.47 | 0.81 | 0.87 |

\sqrt{s} Dependence of Jet Veto

Values with respect to $\sqrt{s} = 14$ TeV

| p_T [GeV] | 12 | | 10 | | 8 | | 6 | |
|---------------|------------------|--|------------------|--|------------------|--|------------------|--|
| | $\epsilon^R(WW)$ | $\frac{\epsilon^R(WW)}{\epsilon^R(Z^*)}$ | $\epsilon^R(WW)$ | $\frac{\epsilon^R(WW)}{\epsilon^R(Z^*)}$ | $\epsilon^R(WW)$ | $\frac{\epsilon^R(WW)}{\epsilon^R(Z^*)}$ | $\epsilon^R(WW)$ | $\frac{\epsilon^R(WW)}{\epsilon^R(Z^*)}$ |
| 20 | 1.07 | 1.04 | 1.10 | 1.04 | 1.16 | 1.08 | 1.25 | 1.11 |
| 25 | 1.06 | 1.03 | 1.08 | 1.04 | 1.14 | 1.07 | 1.21 | 1.09 |
| 30 | 1.05 | 1.03 | 1.08 | 1.04 | 1.12 | 1.06 | 1.18 | 1.08 |
| 35 | 1.04 | 1.03 | 1.06 | 1.03 | 1.11 | 1.06 | 1.16 | 1.08 |
| 40 | 1.04 | 1.03 | 1.06 | 1.03 | 1.10 | 1.05 | 1.15 | 1.07 |
| 45 | 1.04 | 1.02 | 1.05 | 1.03 | 1.09 | 1.05 | 1.13 | 1.07 |
| 50 | 1.03 | 1.02 | 1.05 | 1.03 | 1.08 | 1.04 | 1.12 | 1.06 |
| 55 | 1.03 | 1.02 | 1.05 | 1.02 | 1.08 | 1.04 | 1.11 | 1.06 |
| 60 | 1.02 | 1.01 | 1.04 | 1.02 | 1.07 | 1.04 | 1.10 | 1.05 |
| 65 | 1.02 | 1.01 | 1.04 | 1.02 | 1.07 | 1.04 | 1.10 | 1.05 |
| 70 | 1.02 | 1.01 | 1.04 | 1.02 | 1.06 | 1.03 | 1.09 | 1.05 |
| 75 | 1.01 | 1.01 | 1.03 | 1.02 | 1.06 | 1.03 | 1.09 | 1.05 |
| 80 | 1.01 | 1.01 | 1.03 | 1.02 | 1.05 | 1.03 | 1.08 | 1.04 |
| 85 | 1.01 | 1.01 | 1.03 | 1.02 | 1.05 | 1.03 | 1.07 | 1.04 |
| 90 | 1.01 | 1.01 | 1.03 | 1.02 | 1.05 | 1.03 | 1.07 | 1.04 |
| 95 | 1.01 | 1.00 | 1.03 | 1.02 | 1.04 | 1.03 | 1.07 | 1.04 |
| 100 | 1.01 | 1.00 | 1.03 | 1.01 | 1.04 | 1.02 | 1.06 | 1.04 |

Scale Errors of ZZ/Z*

- Multiply the contribution of gg->ZZ by a factor of 2 (potential QCD NLO K factor) but keep the relative errors at the LO level

Cross-sections in fb

| Mass Range | $\sigma_{q\bar{q}\rightarrow Z^*}^{NLO}$ | | $\sigma_{q\bar{q}\rightarrow ZZ}^{NLO}$ | | $\sigma_{gg\rightarrow ZZ}^{LO}$ | | $\frac{\sigma_{ZZ}}{\sigma_{Z^*}} \times 10^3$ | |
|------------|--|-------|---|-------|----------------------------------|-------|--|-------|
| 200 - 250 | 1858.8 | 4.8 | 8.34 | 4.3 | 3.83 | 62.0 | 6.55 | 12.1 |
| | 1586.8 | -10.5 | 7.14 | -10.6 | 1.50 | -36.4 | 5.45 | -6.7 |
| 250 - 300 | 792.0 | 5.2 | 3.86 | 5.9 | 1.67 | 57.3 | 6.98 | 11.7 |
| | 683.8 | -9.2 | 3.32 | -9.0 | 0.70 | -33.9 | 5.88 | -6.0 |
| 300 - 350 | 390.5 | 4.9 | 1.94 | 4.2 | 0.76 | 53.6 | 6.91 | 9.2 |
| | 340.7 | -8.5 | 1.70 | -8.5 | 0.34 | -31.5 | 5.99 | -5.3 |
| 350 - 400 | 214.7 | 4.4 | 1.10 | 3.3 | 0.39 | 49.3 | 6.97 | 7.7 |
| | 195.3 | -5.0 | 0.96 | -10.0 | 0.18 | -29.8 | 5.87 | -9.3 |
| 400 - 450 | 125.8 | 4.0 | 0.67 | 5.8 | 0.24 | 46.0 | 7.26 | 9.7 |
| | 114.8 | -5.1 | 0.60 | -6.4 | 0.12 | -28.5 | 6.22 | -6.2 |
| 450 - 500 | 79.5 | 4.5 | 0.43 | 6.5 | 0.16 | 44.3 | 7.37 | 9.7 |
| | 72.4 | -4.8 | 0.38 | -6.0 | 0.08 | -26.7 | 6.33 | -5.9 |
| 500 - 750 | 147.6 | 2.6 | 0.78 | 5.9 | 0.32 | 40.9 | 7.47 | 11.3 |
| | 140.4 | -2.5 | 0.70 | -4.8 | 0.18 | -22.0 | 6.27 | -6.5 |
| 750 - 1000 | 28.1 | 2.6 | 0.16 | 2.0 | 0.08 | 30.1 | 8.68 | 7.5 |
| | 28.2 | 2.9 | 0.15 | -4.9 | 0.05 | -17.8 | 7.16 | -11.3 |

